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CMOS TRANS CONDUCTANCE BASED INSTRUMENTATION AMPLIFIER FOR VARIOUS BIOMEDICAL SIGNAL ANALYSIS

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ABSTRACT

The Trans-conductance operational amplifier's operating frequencies are removed using feed forward design approaches. Amplifiers with enormous Trans-conductance that operate in the Giga hertz frequency range are now available to design. Several trans-conductance amplifiers are employed in the design of medical and industrial applications to aid in the processing of biomedical electrocardiographs, and signals such as electroencephalographs, electromyograms, among others. The proposed study demonstrates the design of an instrumentation amplifier based on CMOS and the processing of biomedical ECG, EEG, and EMG signals using Trans-conductance operational amplifiers. The CMOS manufacturing technique allows sophisticated circuits to be integrated on a small surface area. Noise reduction, low DC offset, high output impedance, and Common Mode rejection Ratio values are all aspects of the Trans-conductance instrumentation operational amplifiers. Electronic Design and Automation tool with 0.13m CMOS process technology was used for circuit implementation and simulations.

Keywords : Trans-conductance; Instrumentation Amplifier; CMOS Process; Biomedical Signals; Bio-potential Signal; CMRR; Frequency response; Signal Measurement

I. Introduction

A high performance CMOS instrumentation amplifier design becomes a popular choice for biomedical circuit design as such designs offers low voltage, low power operating parameters and minimal chip area for component integration. [1-3], [5-6], [9] Biomedical signals also known as bio-potentials [7]. These electrical impulses have a low frequency and a low amplitude. As a result, some type of amplifier circuit is required to accomplish the amplification process for these weak electrical bio potentials. The bio potential amplifier is the amplifier used in the bio potential amplification process. [7-8], [9], [17].

There are numerous types of bio potential amplifiers, such as differential, isolation, operational, and chopper amplifiers [8]. These amplifiers are designed to work with low-frequency and low-voltage biopotentials. Amplifiers must have a high input impedance value, among other requirements. The input impedance of these amplifiers must be at least 100M Ω . Because bio potentials have lower frequencies and only range from Hz to kHz, these biopotential amplifiers should be able to work in the low-frequency range. These amplifiers should be designed with

suitable protection and isolation subcircuits to avoid any artifacts and mismatch, and they should give large gain values so that the weak amplitude biopotentials may be easily visible on display devices.

Circuits using differential amplifiers and operational amplifiers are chosen over alternative bio potential amplifiers in bio medical circuit design. Differential amplifiers can filter out interference or common mode signals from electrodes attached to the human body that are used to capture heart movements. As a result, differential amplifiers have a high CMRR value. Differential amplifier also provides good stability [7-8]. Though such amplifier circuit has better ability for interference rejection but it lacks having enough input impedance. To overcome the limitation of the value of input impedance and to achieve large CMRR value operational amplifier based instrumentation amplifier is used in bio potential amplifier circuit implementation.

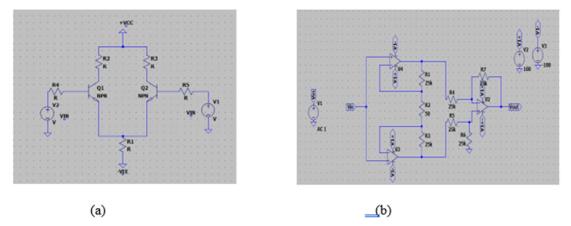


Figure 1 (a) Differential Amplifier schematic (b) Instrumentation Op-Amp schematic

Trans-conductance Operational Amplifiers

Trans-conductance operational amplifier [10], [14], [19] or OTA provides wide signal bandwidth for many amplifier circuits. In this amplifier, input voltage that is applied at the opamp produces output current. There is an additional amount of current present that controls the trans-conductance of operational amplifier.

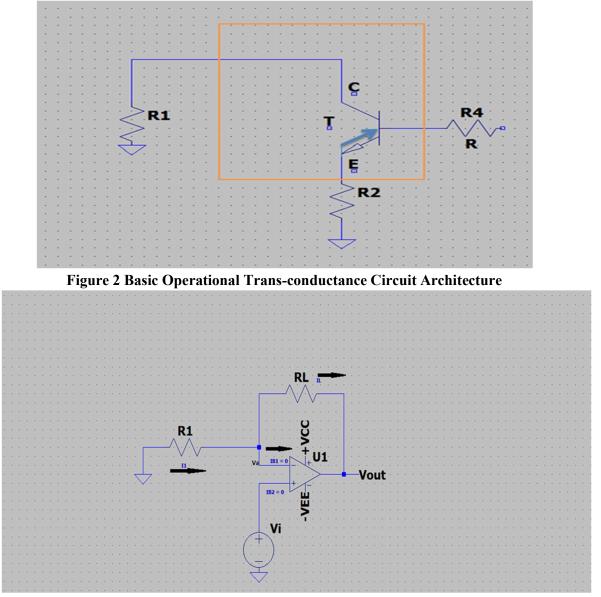


Figure 3 Trans-conductance Operational Amplifier

From figure 3, the equation for the output current from this circuit is given as

At point 'a'

 $V_{a} = V_{i}$ ------ (1) And $I_{B1} = I_{B2} = 0$ ------ (2)

Using Kirchhoff's current law, we have

Copyright © 2022. Journal of Northeastern University. Licensed under the Creative Commons Attribution Noncommercial No Derivatives (by-nc-nd). Available at https://dbdxxb.cn/ $I_1 = I_{B1} + I_L$ ------ (3)

From equation (2)

 $I_1 = I_L$

Current through Resistor R1 is given by equation

$$I_1 = \frac{V_i}{R_1}$$

II. Literature Survey

A two stage op-amp based CMOS instrumentation amplifier has been presented using 0.13 μ m CMOS fabrication technology [17]. The proposed circuit design is able to reduces the power dissipation by scaling down the supply voltage. The circuit is able to work on single power supply of 1.8 volt. The circuit design has three subsections where the first stage is differential gain, an additional gain stage and a bias string being an intermediate stage and last stage for the proposed circuit design respectively. Large value of circuit gain is achieved due to these three op-amp subsections. The overall current gain of 21.18dB with 6.32 MHZ unity gain bandwidth has been achieved from this proposed circuit.

Low amplitude ECG signals are more prone to interference in ECG recorder devices. Such interferences mainly caused by power line of the recording devices. A novel circuit implementation has been proposed which reduces such power line interferences and provide large CMRR and more gain [14]. The circuit provides reduction in power consumption of the circuit and input noise. The amplifier parameters such as CMRR of 135db, a voltage gain of value 41.8db and power consumption of 4.32 μ W is achieved from proposed circuit implementation.

A 3 op-amps based current mode instrumentation amplifier has proposed [11]. The current mode topology is based on power supply current sensing techniques. Three commonly used current sensing techniques are based on inductor's resistance, MOSFETS and on sense resistors.

A three op-amp cascade structure has limited performance due to characteristics mismatch and issues in current mirror such as threshold voltage and process variations. The proposed circuit implementation solved these issues by utilizing the sense resistor in op-amp structure. The amplifier provides a CMRR of value 130db for the 87 Hz bandwidth and 93db gain. The circuit is well operated at 1.8 volt single power supply.

An OTA based CMOS IA is proposed for a biomedical application [12]. The three inputs OTA is belonging to voltage controlled current source. The proposed circuit has achieved large CMRR and PSRR with values 124db and 65bd respectively, low dc offset 0.3mVolts. The circuit shows power consumption of 0.52 mW.

III. Instrumentation Amplifiers

Development of efficient instrumentation amplifier [11], [12] in CMOS fabrication process has a number of advantages, including lower voltage and power requirements, more noiseresistant devices, the ability to incorporate complicated circuitry on a single silicon chip, and simple trans-conductor implementation. It is an integrated circuit that is used to amplify extremely weak signals. It is utilised in biomedical systems to correctly monitor bio potential signals since it is more resistant to noise removal. The following are significant properties of an instrumentation amplifier:

Stable and accurate gain High CMRR High value input impedance, low value output impedance High slew rate

Traditional Instrumentation amplifier using 2 stage op- amp circuits is given below. It consists of two inverting and non-Inverting op-amps at the input stage and one output op-amp.

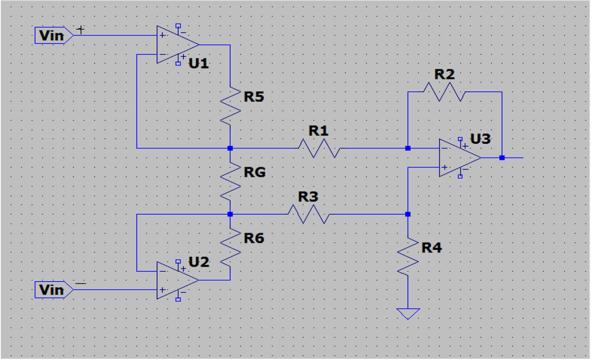


Figure 4 Traditional 2 stage Op-Amp Instrumentation Amplifier

The output voltage from the circuit shown in figure 4 is given by

$$V_{out} = \frac{R_2}{R_1} \left(\frac{2R_5}{R_G} + 1 \right) (Vin_+ - Vin_-)$$

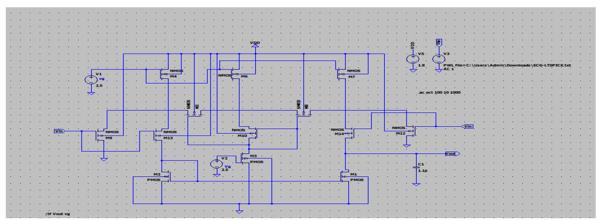


Figure 5.1 OTA Based CMOS Amplifier

IV. Implementation

The proposed work is concerned with testing the capability of an OTA-based instrumentation amplifier. Figure 5.1 depicts the schematic of an OTA-based CMOS amplifier. Three different bio-potential source signals are used for this purpose: ECG, EEG, and EMG. The piecewise linear voltage files are fed into an instrumentation amplifier's input. These source signals' amplification is investigated. In the same way, some common mode noise signals are mixed in with these source signals.

Figure 5.2 depicts the proposed circuit implementation, which employs three wideband OPA861 operational trans-conductance amplifiers. Two OTAs are used to build a differential amplifier input stage. The remaining trans-conductance amplifier is used to reverse the current. The current flowing through the differential amplifier is out of phase with the current flowing through capacitor C. For current collection, an op-amp-based integrator is used. An RC circuit is connected to avoid propagation delay.

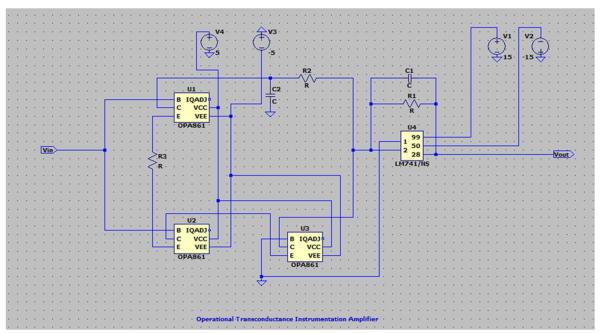


Figure 5.2 OTA Based Instrumentation Amplifier



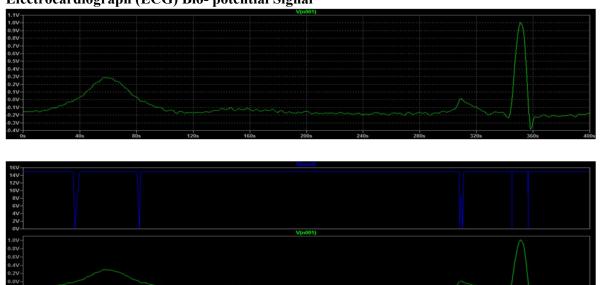


Figure 6.1 Input ECG Signal Source

ECG signal having amplitude ranging from -400 mv to 900 mv is applied to proposed instrumentation amplifier and output at a range of 14 volt is observed at the output of the instrumentation amplifier.

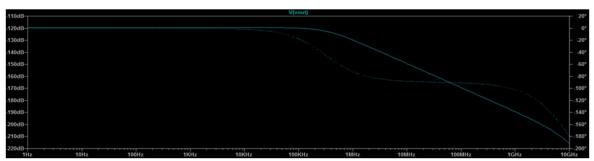


Figure 6.1.1 Frequency Response Curve of OTA Instrumentation Amplifier in Differential Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Differential mode ranging from 1Hz to 1GHz is plotted with maximum gain up to 120db is obtained.

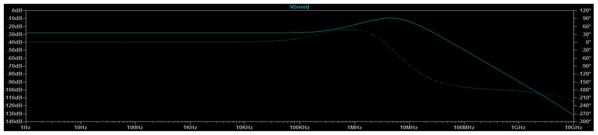
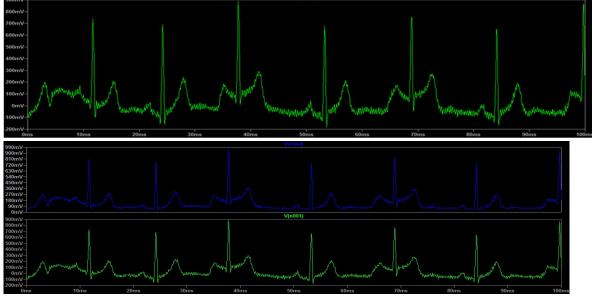


Figure 6.1.2 Frequency Response Curve of OTA Instrumentation Amplifier in Common Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Common mode ranging from 1Hz to 10GHz is plotted with maximum gain up to -10db is obtained.



Electroencephalography (EEG) Bio- potential Signal

Figure 6.2 EEG Signal Source

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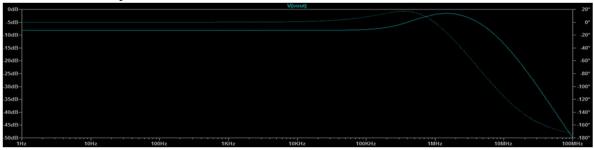


Figure 6.2.1 Frequency Response of OTA Instrumentation Amplifier in Common Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Common mode ranging from 1Hz to 100MHz is plotted with maximum gain up to -2db is obtained.

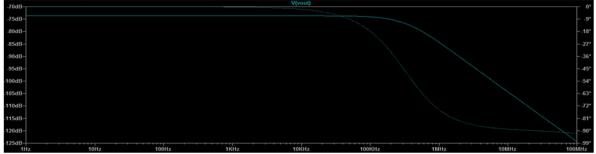
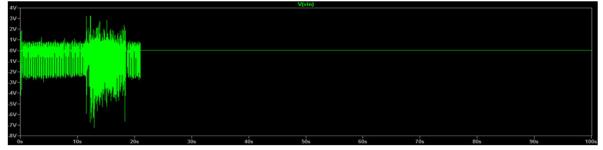


Figure 6.2.2 Frequency Response of OTA Instrumentation Amplifier in Differential Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Differential mode ranging from 1Hz to 100MHz is plotted with maximum gain up to -75db is obtained.

Electromyography (EMG) Bio- potential Signal



2.0V- 1.5V- 1.0V- 0.5V-	Lateland			V(n001)					
2.0V 1.5V 0.5V 0.5V 0.5V 1.0V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V 0.5V 1.5V	a di								
-3.5V -4.0V 16V									
14V-									
12V- 10V- 8V- 6V-									
4V- 2V-									
0V-									
-2V-	10s 20s	30s	40s	50s	60s	70s	80s	90s	100s

Figure 6.3 Input EMG Signal Source

EMG signal having amplitude ranging from -1mv to 1500 mv is applied to proposed instrumentation amplifier and output at a range of 14 volt is observed at the output of the instrumentation amplifier.

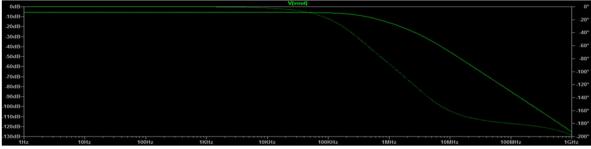


Figure 6.3.1 Frequency Response of OTA Instrumentation Amplifier in Differential Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Differential mode ranging from 1Hz to 1GHz is plotted with maximum gain up to -10db is obtained.

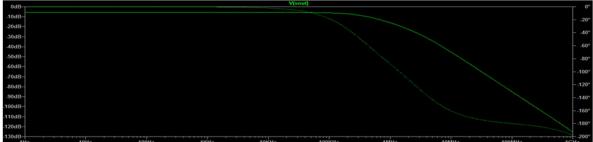


Figure 6.3.2 Frequency Response of OTA Instrumentation Amplifier in Common Mode Configuration

Frequency response of the proposed OTA instrumentation amplifier at Common mode ranging from 1Hz to 100MHz is plotted with maximum gain up to -1db is obtained.

Instrumentation Amplifier Parameters	ECG Bio-potential	EEG Bio-potential	EMG Bio- potential
CMOS Technology	0.13 μm	0.13 μm	0.13 μm
Supply Voltage	1.8 V	1.8 V	1.8 V

VI. Observation Table

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Power Consumption	0.09 W	0.09 W	0.09 W	
CMRR (DC)	54 dB	54 dB	54 dB	
-3 db frequency BW for Differential signals	364.58 KHz	415.447 KHz	217.711 KHz	
-3 db frequency BW for Common Mode signals	8.9724 MHz	674.8541 KHz	293.54 MHz	

 Table 1 Instrumentation Amplifier Parameter Values for Bio-potential Signals

VII. Conclusion

The operational Trans conductance amplifier based instrumentation amplifier has been implemented to analyze EGC, EEG and EMG bio potential signals. An instrumentation amplifier implemented has wideband OTAs with CMRR of value 54 dB and slew rate of 900 v/ μ s with operating bandwidth of 80 MHz The cut off frequency for ECG, EEG and EMG signals are measured as 364.58 KHz, 415.447 KHz and 217.711 KHz respectively. Operational Trans-conductance amplifier based instrumentation is suitable for such bio potentials analysis.

VIII. Future Scope

Future emphasis should be placed on improving the value of CMRR, as well as the implementation of complex bio-potential signals such as EEG and EMG bio-potential signals.

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